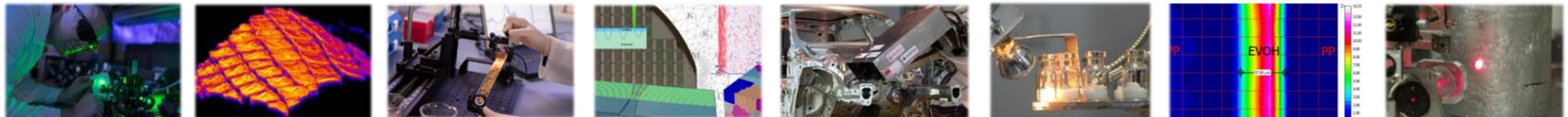


Measurement and calculation of sound velocities of steel during recrystallisation

Clemens Grünsteidl¹, Christian Kerschbaummayr¹, Klarissa Meirer¹, Georg Watzl¹, Martin Rzyzy¹, Edgar Scherleitner¹, Matthias Militzer³, Christian Hoflehner², Markus Sonnleitner²

LUS4Metals, 22.05.2024, Stockholm

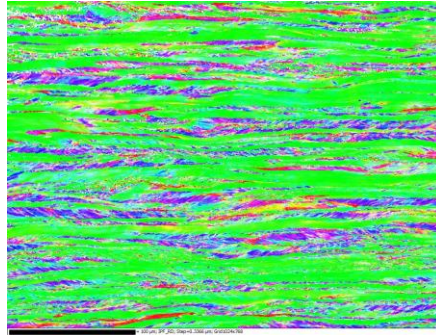


Cold rolled steel sheets

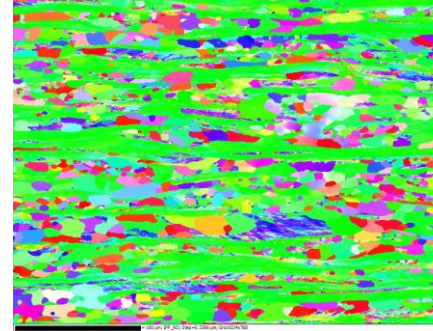
- Shape of grains:
- Orientation of grains:

Elongated grains → Equiaxed grains
Rolling texture → Recrystallized texture

0% REXX



50% REXX at 640°C



100% REXX at 700°C



Technical importance: Forming behavior



Engler and Randle, V., 2008, *Introduction to Texture Analysis : Macrotexture, Microtexture, and Orientation Mapping*.

Why LUS for Recrystallization?

- State of the art methods: **direct**,
ex-situ, **slow**

Micrographs, Electron back scatter diffraction (EBSD), Microhardness, ...

- Laser Ultrasound: **in-situ**, **fast**,
indirect

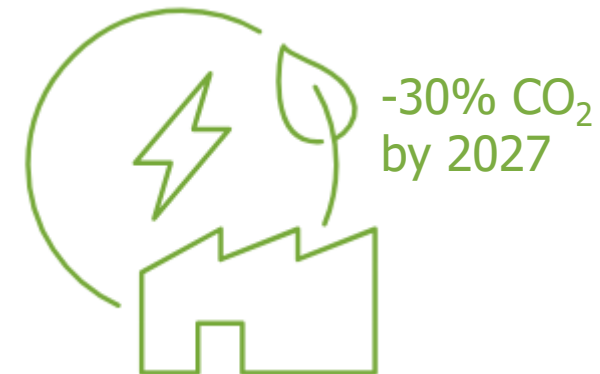
Sound velocities, attenuation

Electric arc furnace and scrap metal recycling

- Tramp elements in scrap metal
- Many characterization measurements

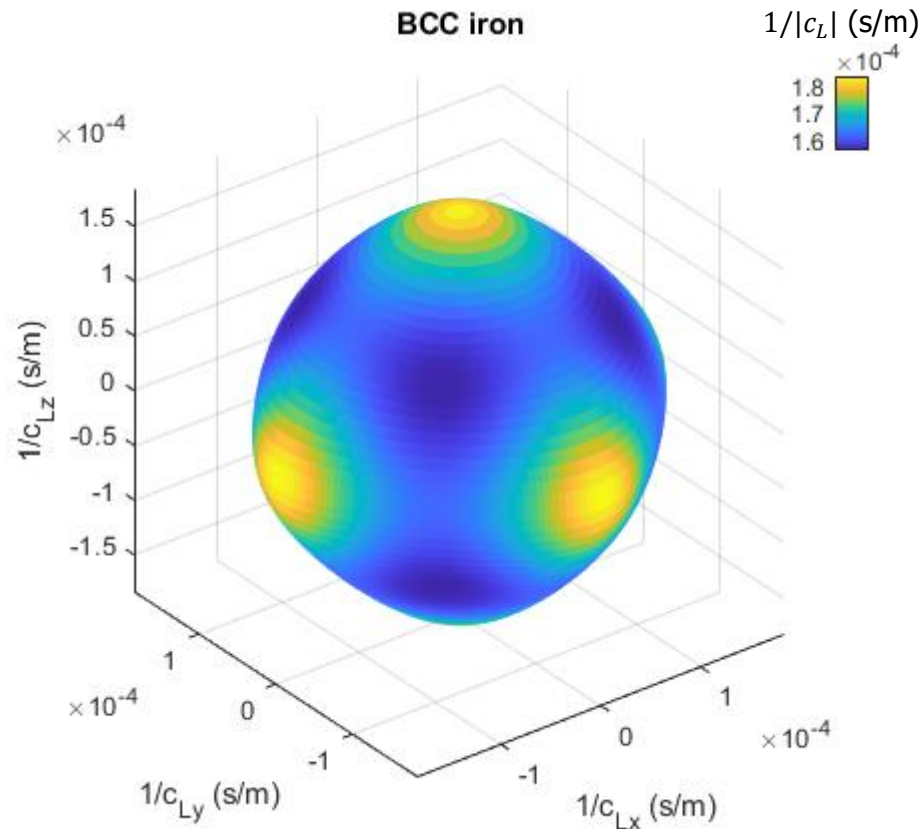


© voestalpine.com



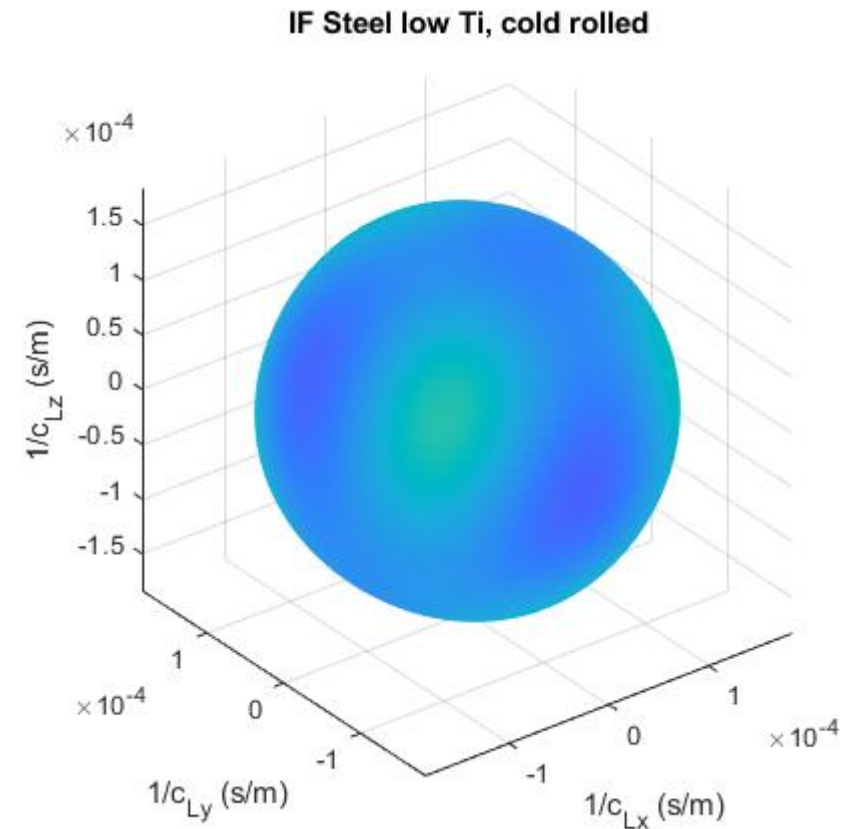
- Single crystal iron

Directional dependence of sound velocities



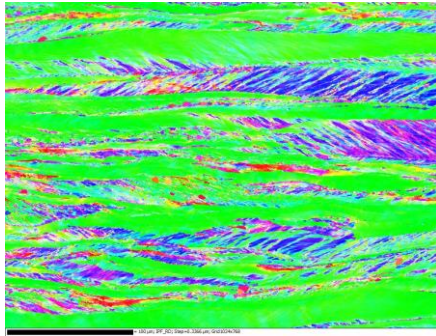
- Polycrystalline iron with texture

Non uniform orientation distribution of grains

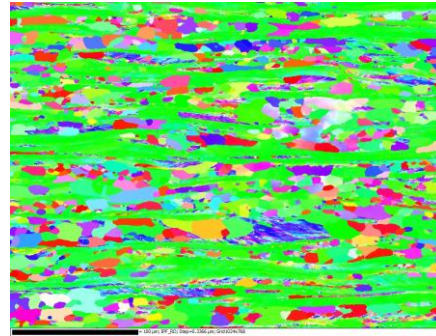


Change of grain orientation distribution

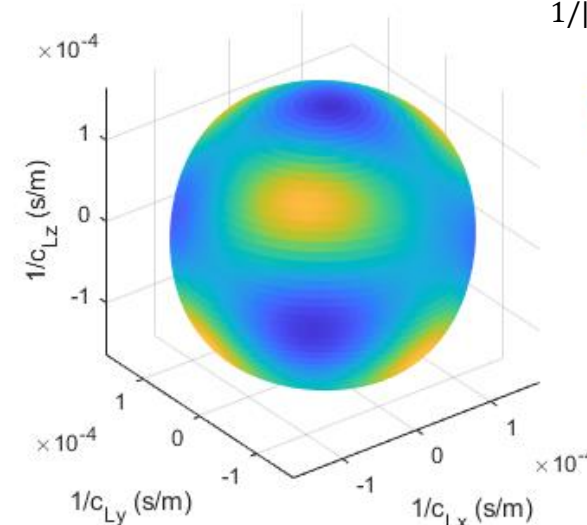
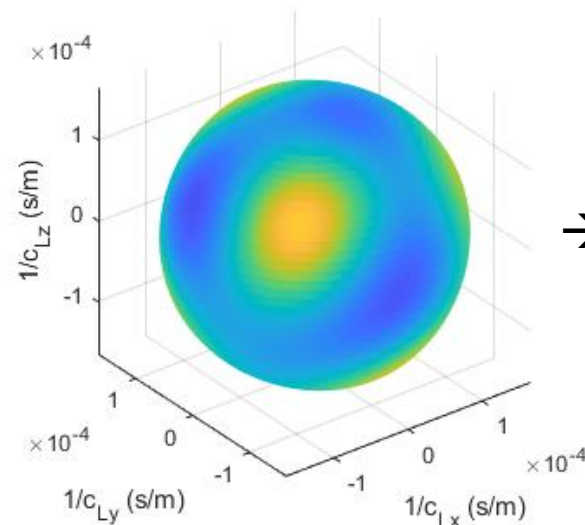
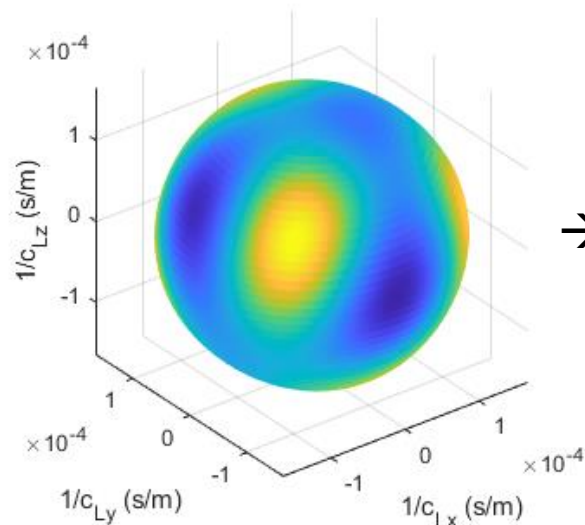
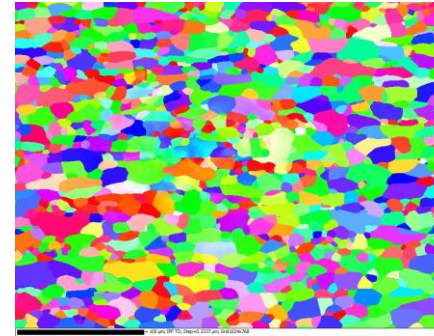
0% at 600°C



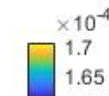
50% at 640°C



100% at 700°C



$1/|c_L|$ (s/m)



~2% change of c_L
in normal direction

- Homogenized elastic stiffness tensor:

rotated single crystal stiffness tensor ($C(T)$ from *Dever, D. J., 1972*)
 $\overbrace{C(\varphi_1, \Phi, \varphi_2)}$

- Homogenized elastic stiffness tensor:

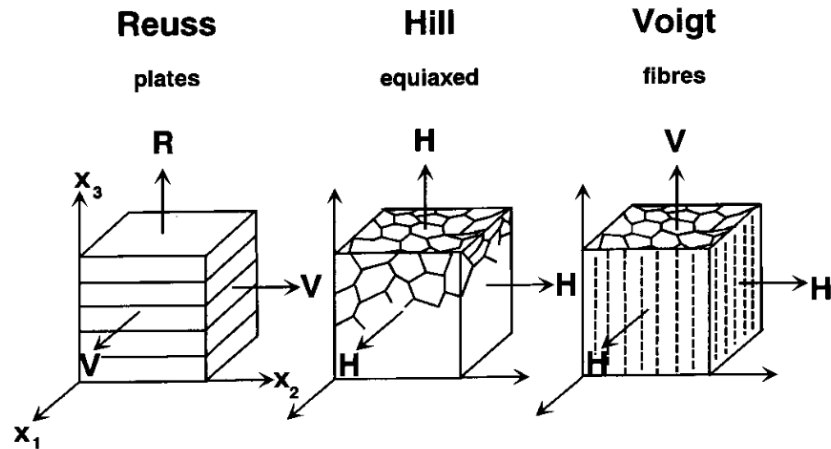
$$\underbrace{f(\varphi_1, \Phi, \varphi_2)}_{\text{orientation density (from EBSD)}} \underbrace{C(\varphi_1, \Phi, \varphi_2)}_{\text{rotated single crystal stiffness tensor } (C(T) \text{ from } \textit{Dever, D. J., 1972})}$$

- Homogenized elastic stiffness tensor:

$$C_{Voigt} = \frac{4}{\pi^2} \underbrace{\int_0^{\frac{\pi}{2}} \int \int f(\varphi_1, \Phi, \varphi_2) C(\varphi_1, \Phi, \varphi_2) \sin(\Phi) d\varphi_1 d\Phi d\varphi_2}_{\text{Integral over Euler Space (all Orientations)}}$$

- Homogenized elastic stiffness tensor:

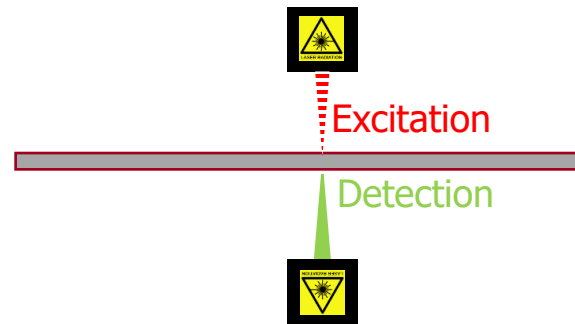
$$C_{Voigt} = \frac{4}{\pi^2} \int_0^{\frac{\pi}{2}} \int_0^{\frac{\pi}{2}} \int_0^{\frac{\pi}{2}} f(\varphi_1, \Phi, \varphi_2) C(\varphi_1, \Phi, \varphi_2) \sin(\Phi) d\varphi_1 d\Phi d\varphi_2$$



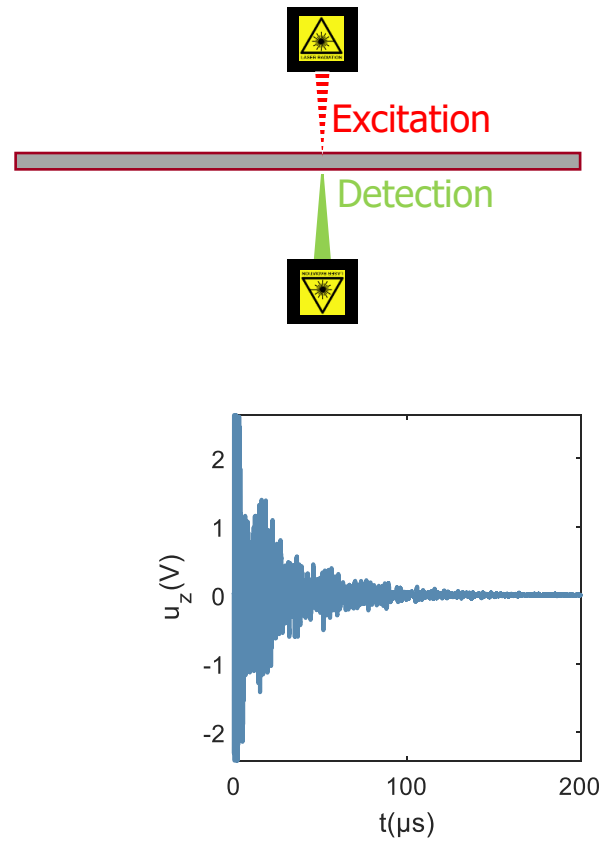
- C_{Voigt} and C_{Reuss} : Theoretical limits
- Combinations: $C_{VR} = w C_V + (1 - w)C_R$
- solve wave equations → sound velocities

Bunge et al., 2000, "Elastic Properties of Polycrystals - Influence of Texture and Stereology," J. Mech. Phys. Solids, **48**(1), pp. 29–66.

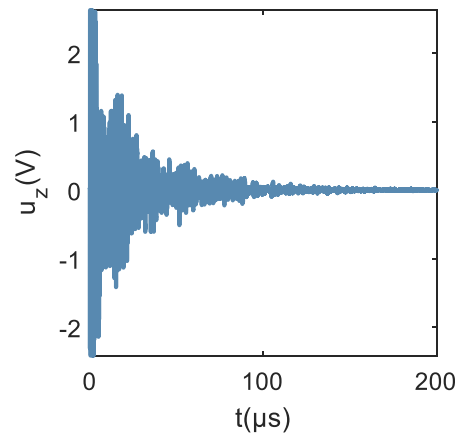
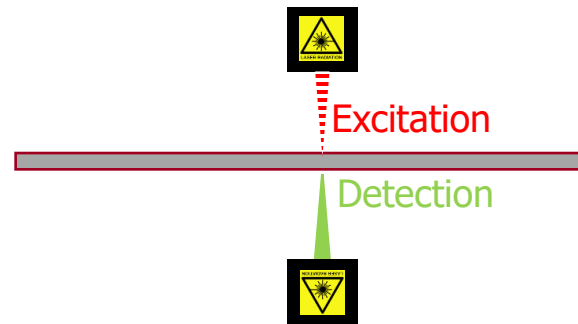
Measurement of plate resonances



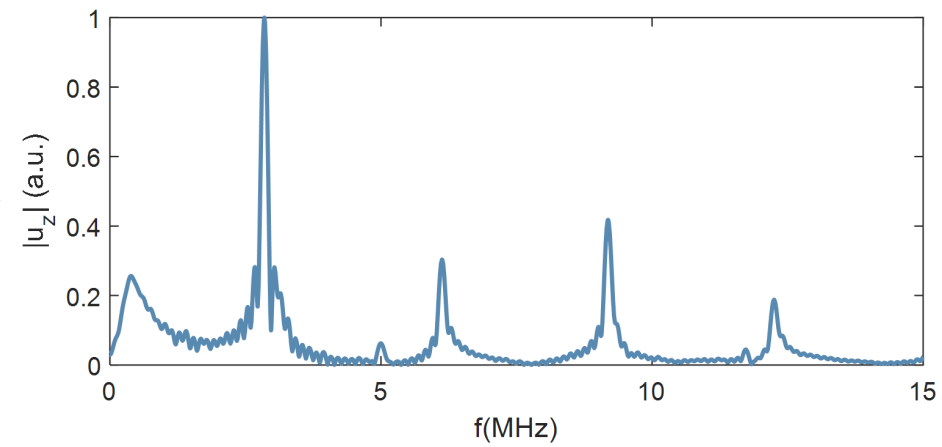
Measurement of plate resonances



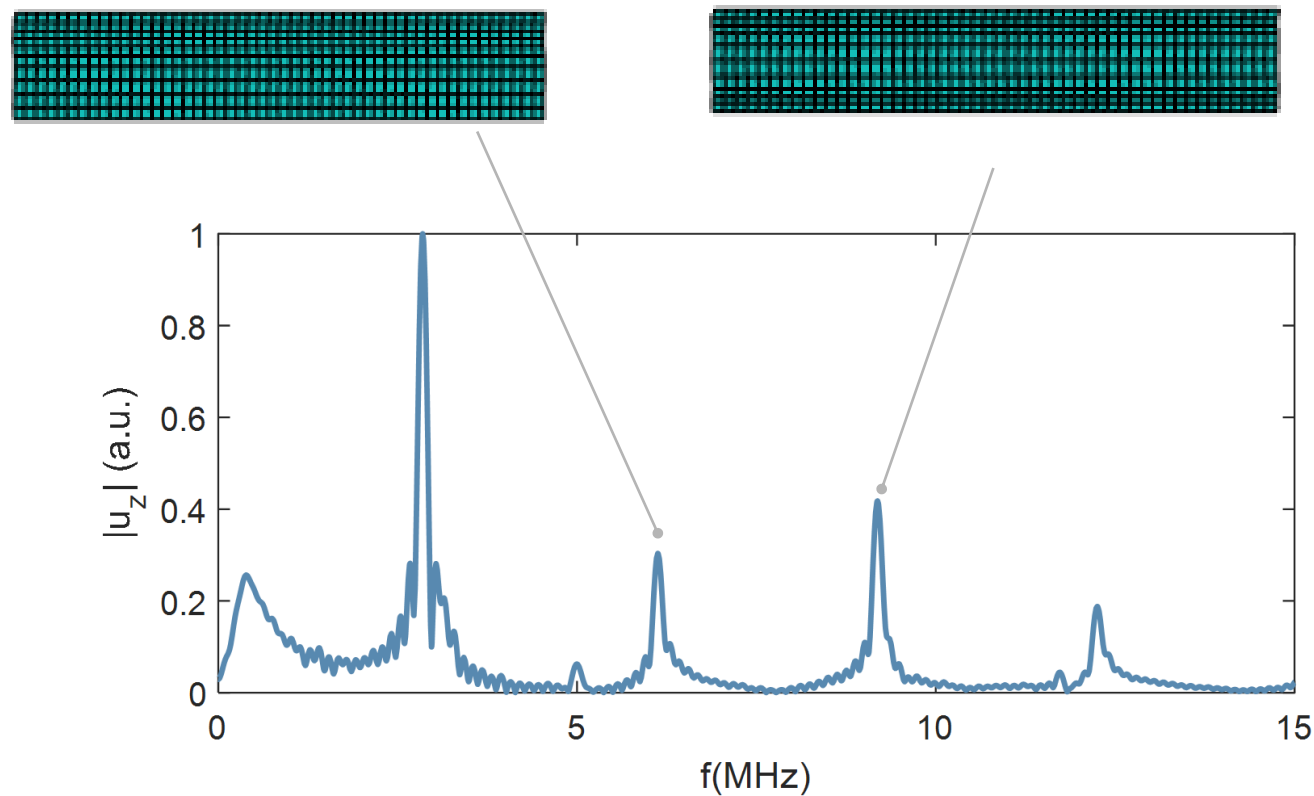
Measurement of plate resonances



FFT

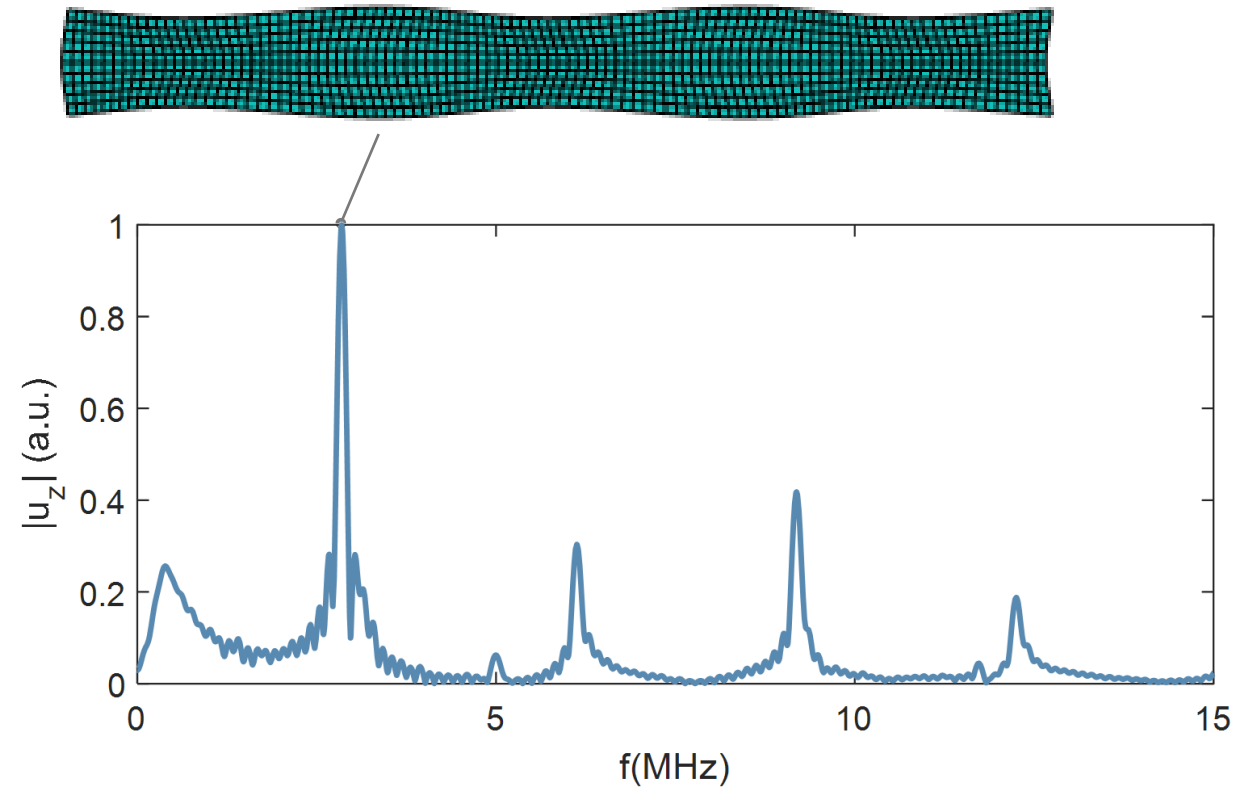


thickness-resonances: standing plane waves at $f_L = n \frac{c_L}{2h}$



Measurement of plate resonances

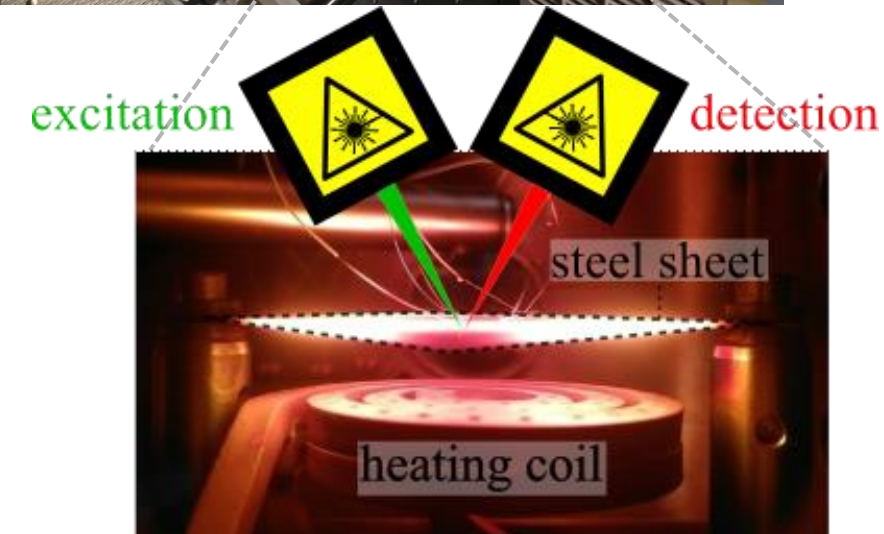
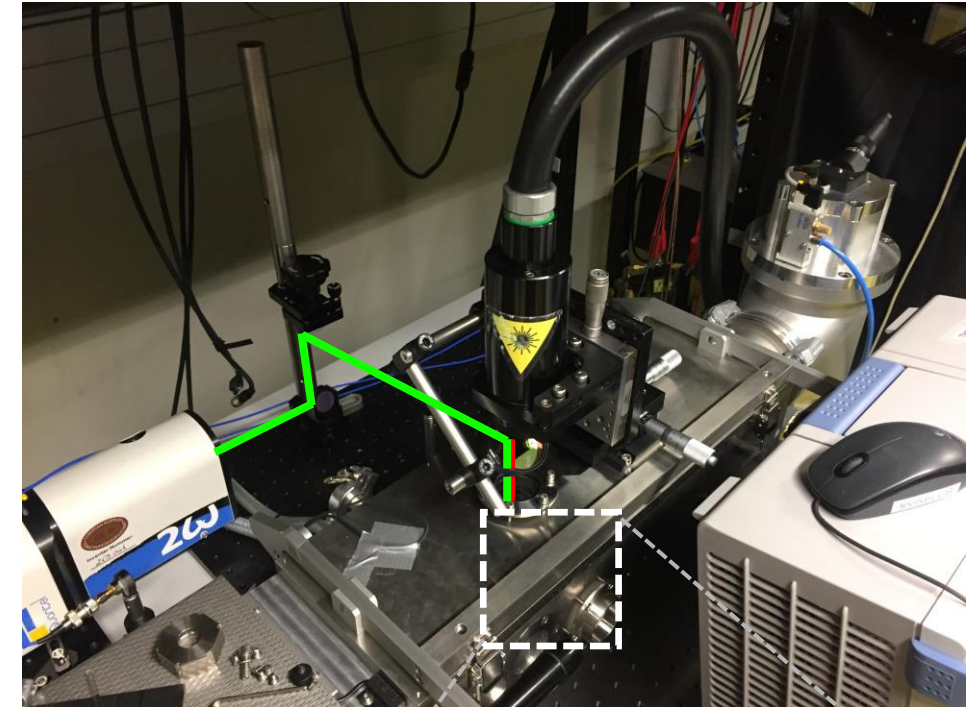
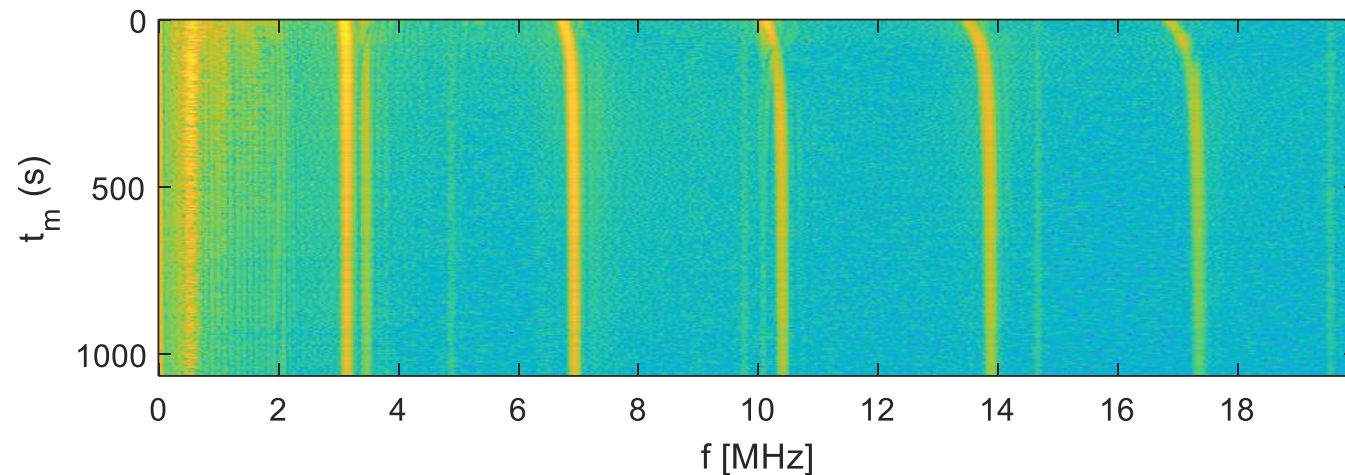
Largest: Zero-Group-Velocity resonance



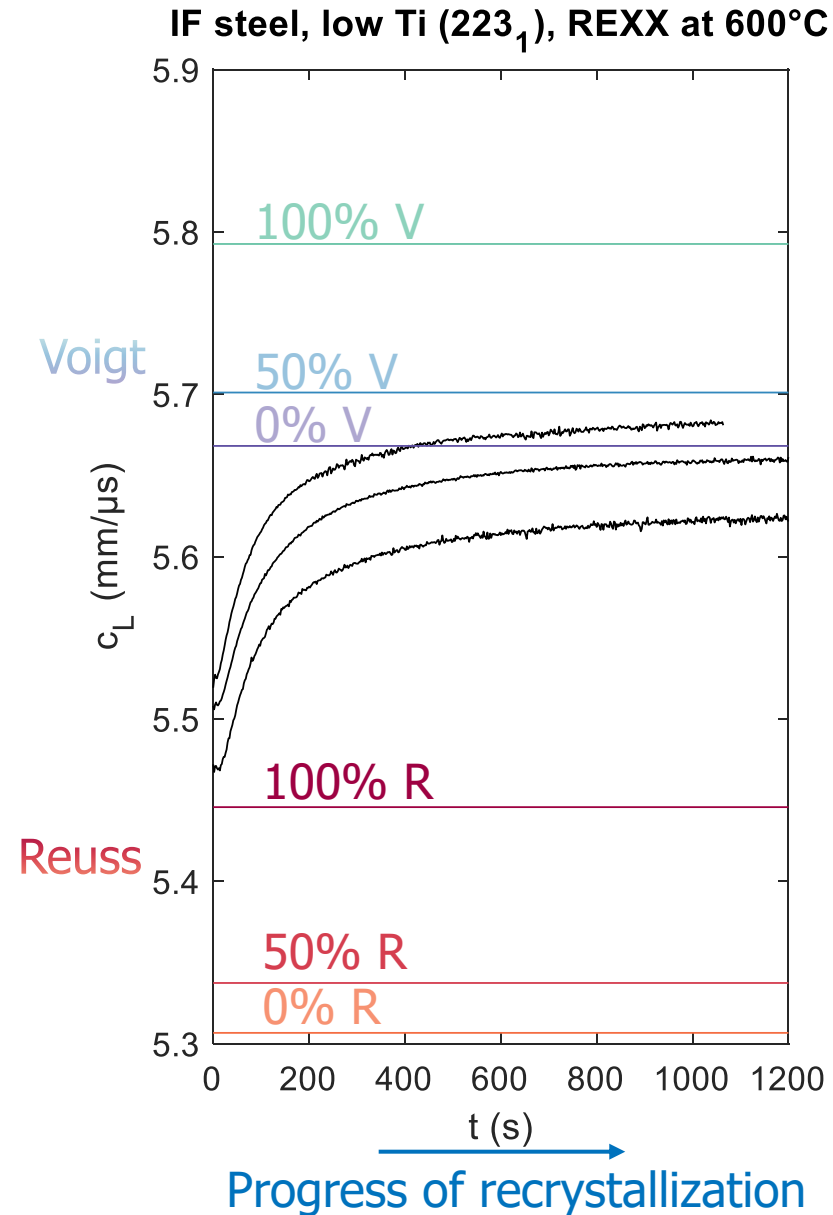
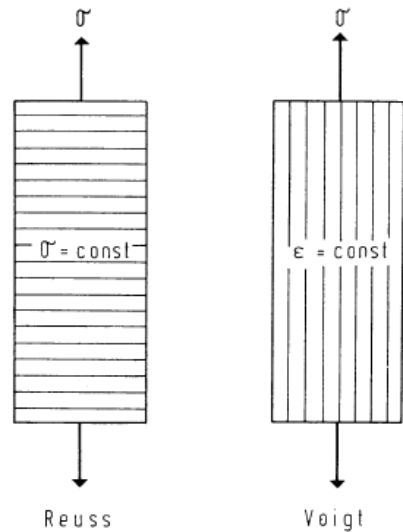
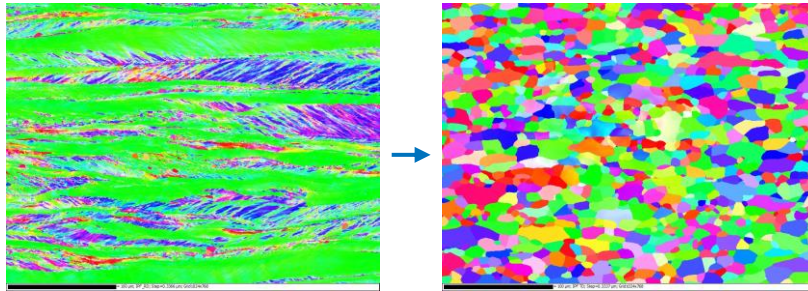
Measurement in thermal simulator

- Linseis Dilatometer, LUS coupled through windows
- Detection: TECNAR PDL (1064nm, 10Hz, 30mJ)
- Generation: Quantel Q-Smart 850 (532nm, 10Hz, 100mJ)

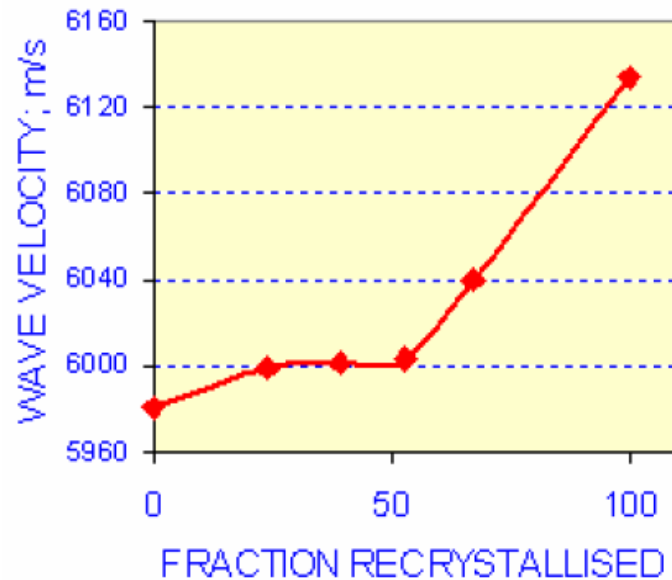
In situ during recrystallisation at 600°C:



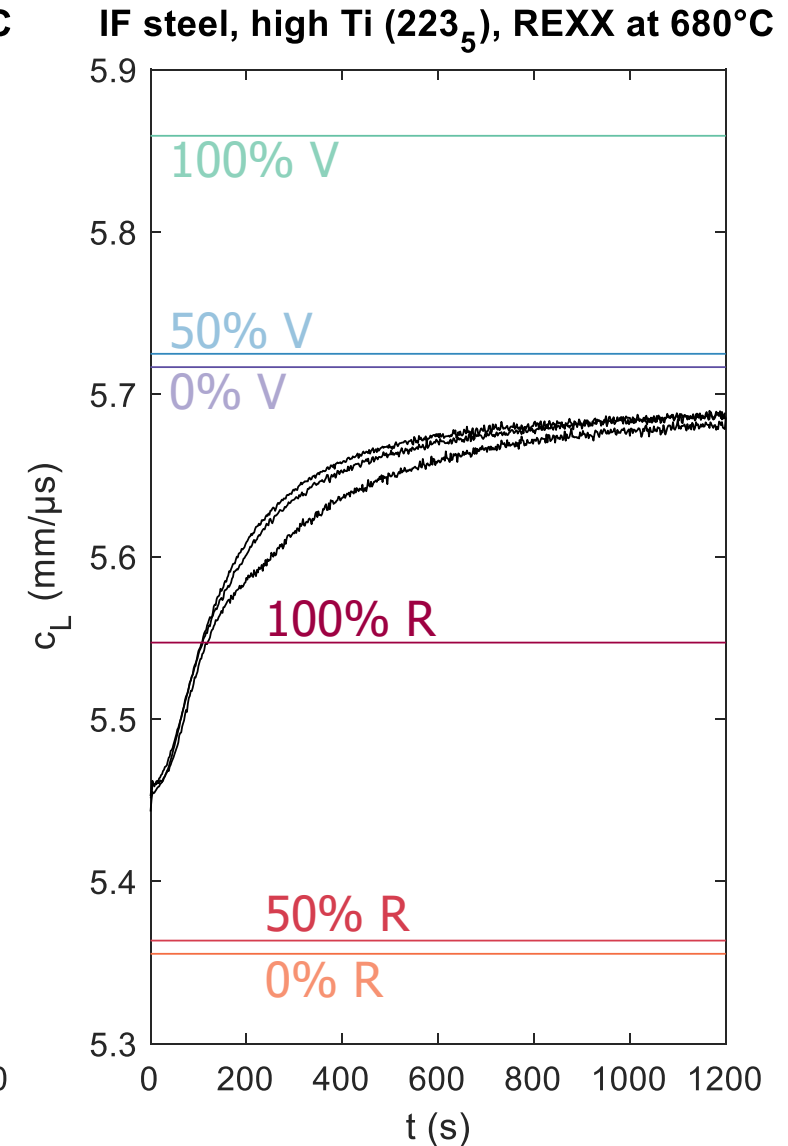
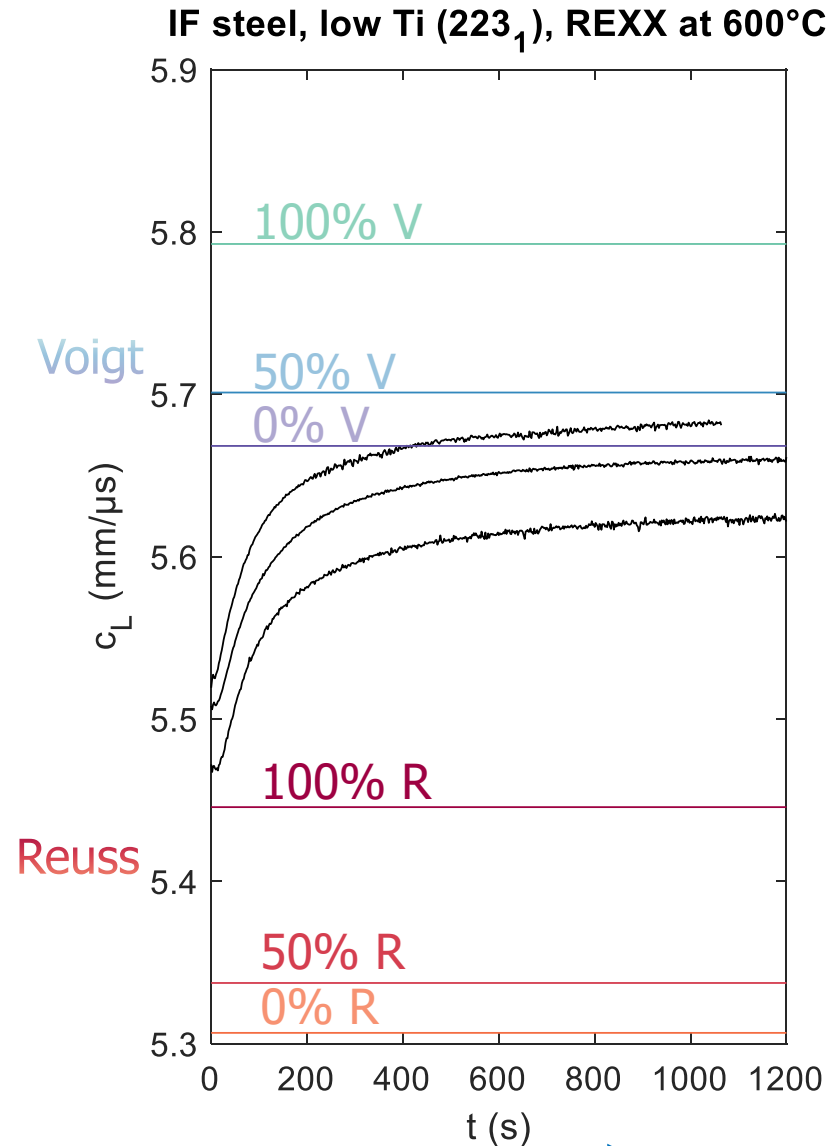
Calculated vs. measured c_L



Calculated vs. measured c_L



Hutchinson et al., 2008, "Application of Laser Ultrasonics to Studies of Recrystallisation and Grain Growth in Metals," Technology, pp. 2–7.

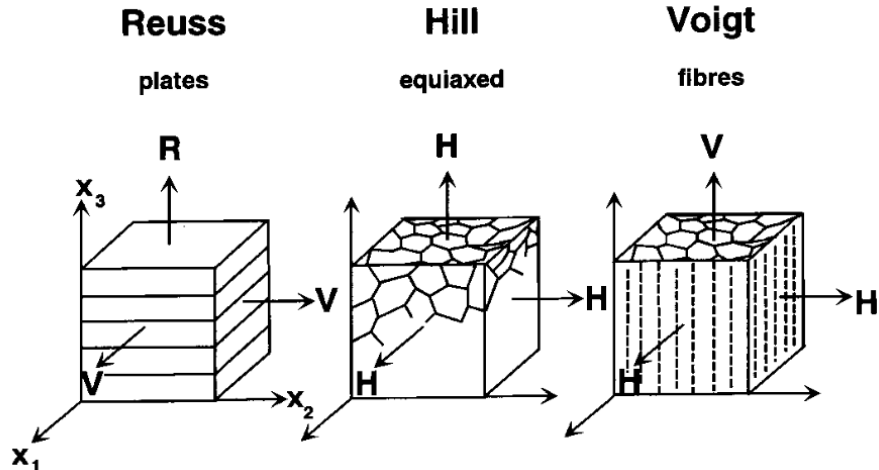


Progress of recrystallization

Combine Voigt and Reuss:

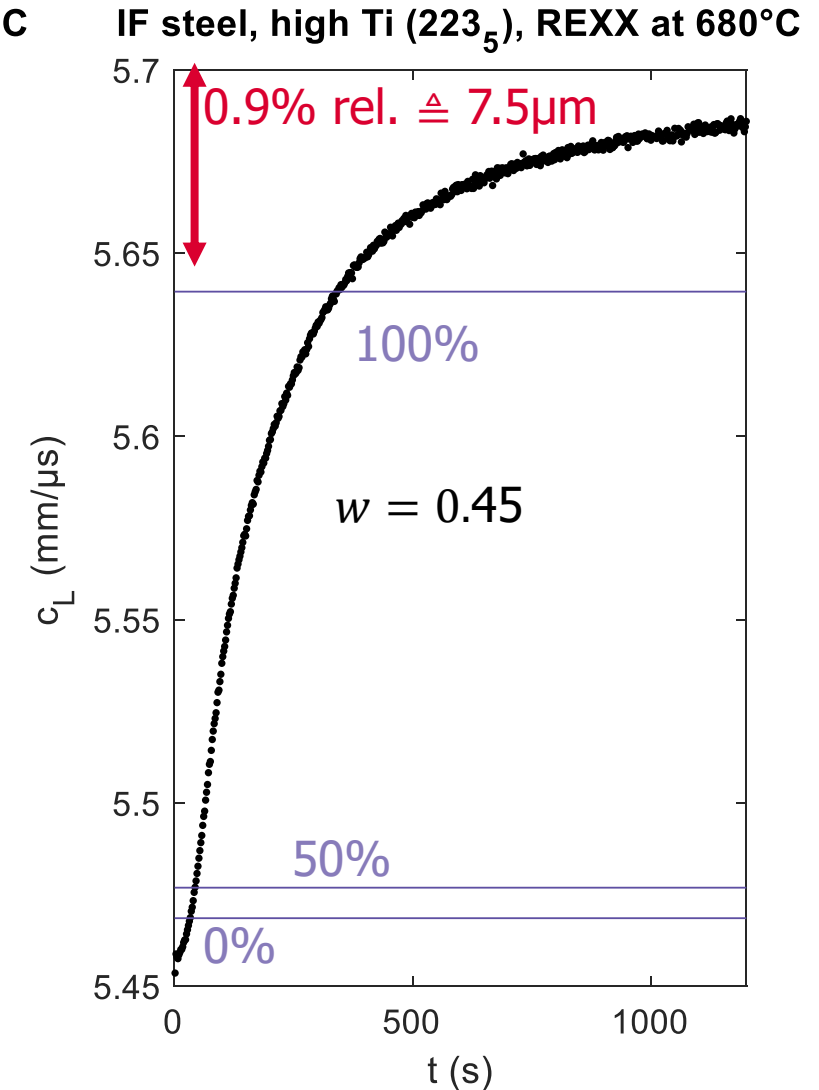
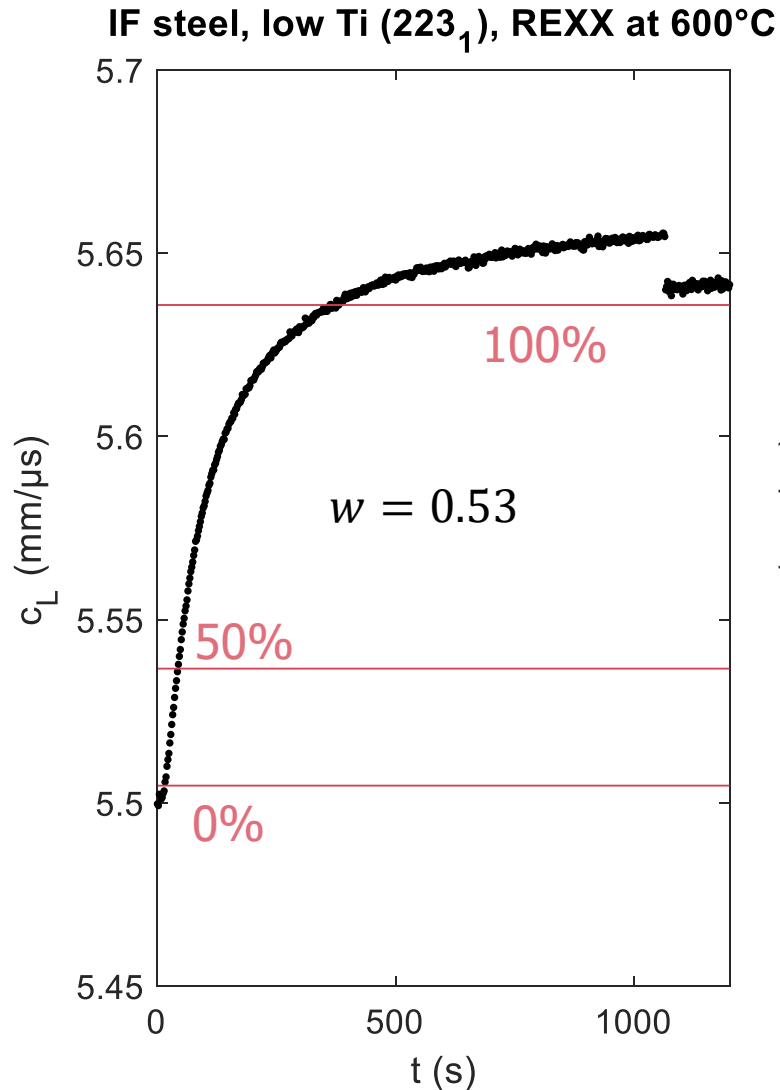
$$C_{VR} = w C_V + (1 - w)C_R$$

Reuss $\rightarrow$ Voigt? Change of w ?



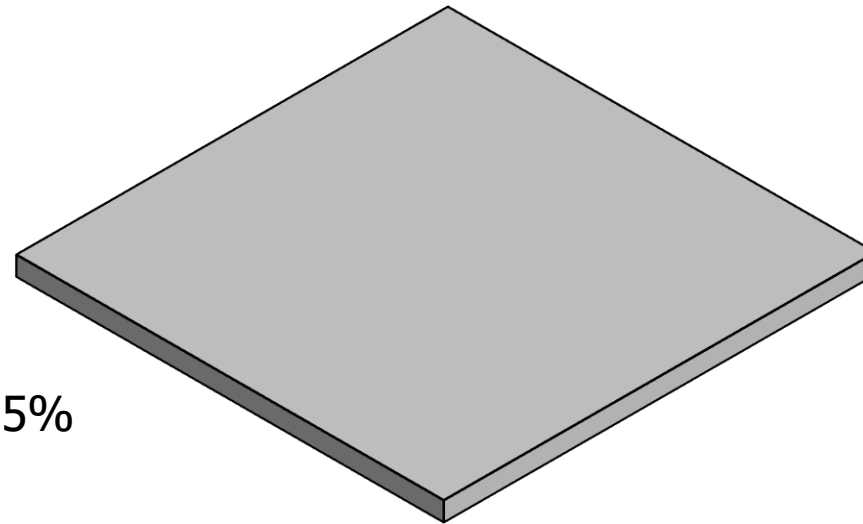
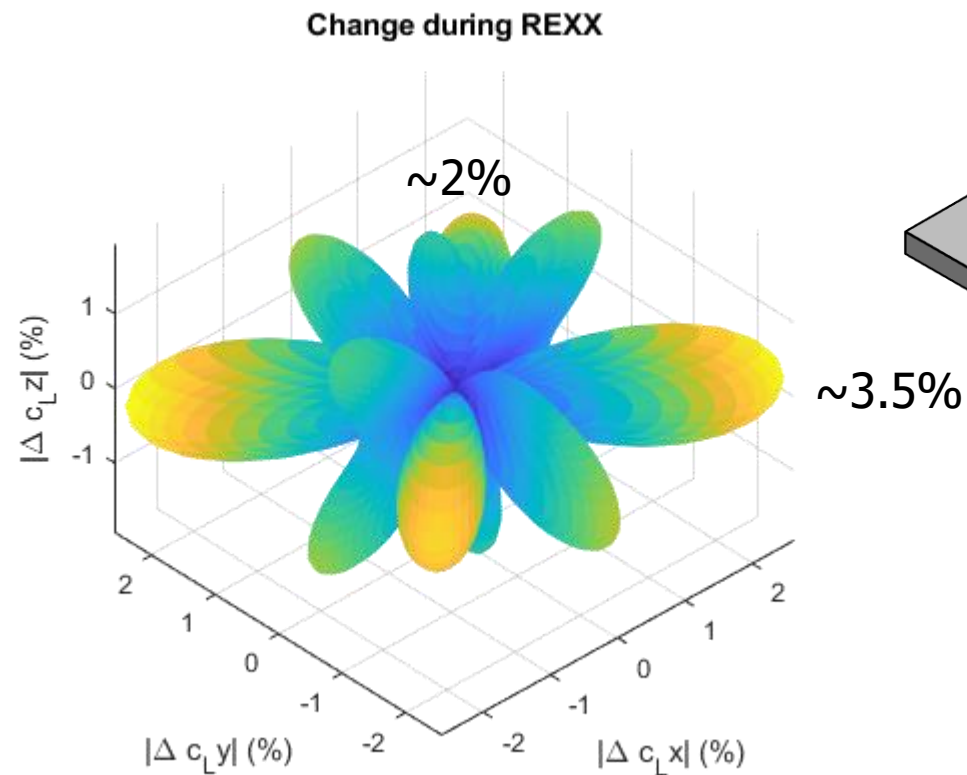
Bunge et al., 2000, "Elastic Properties of Polycrystals - Influence of Texture and Stereology," J. Mech. Phys. Solids, **48**(1), pp. 29–66.

mean results

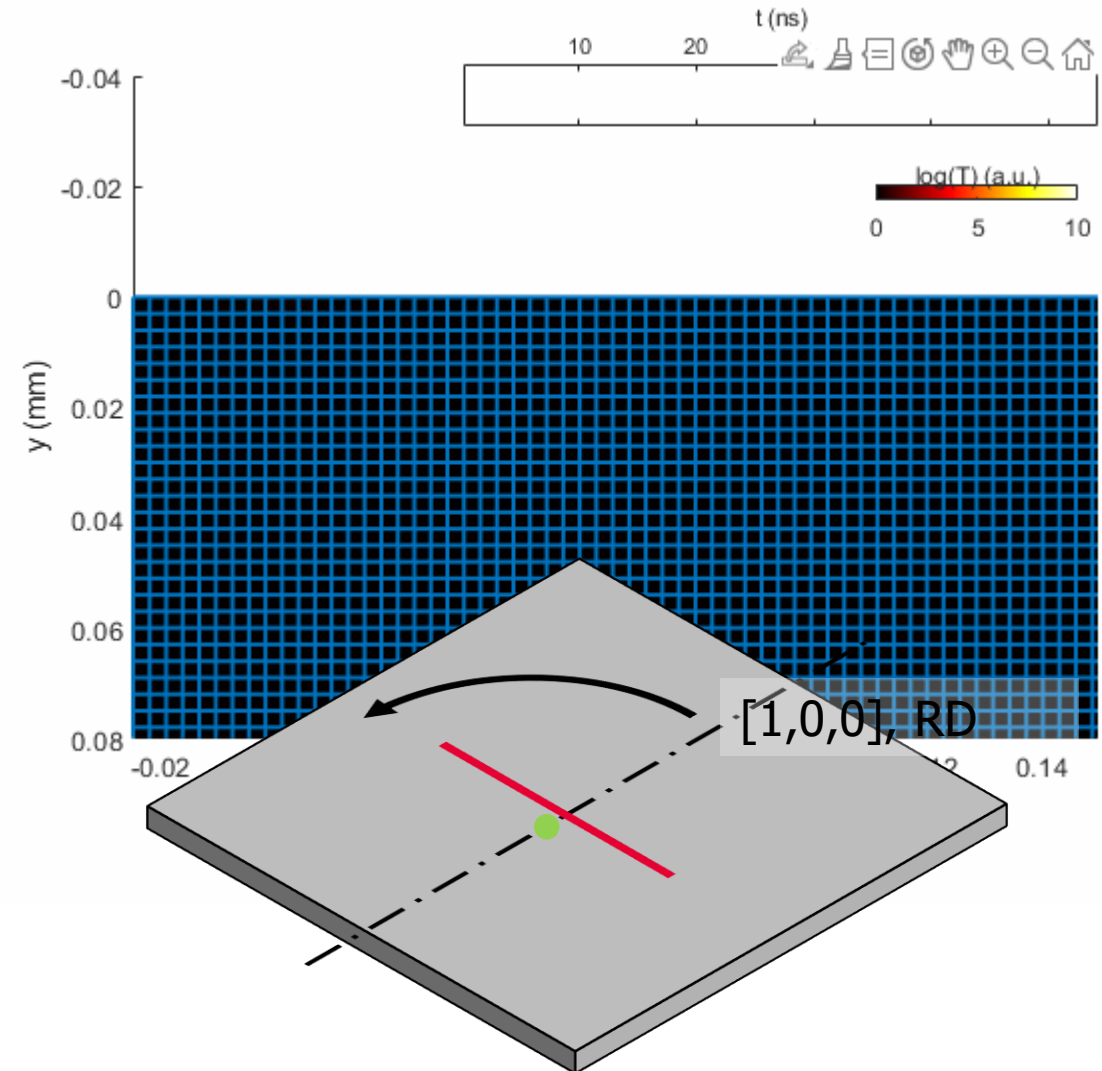


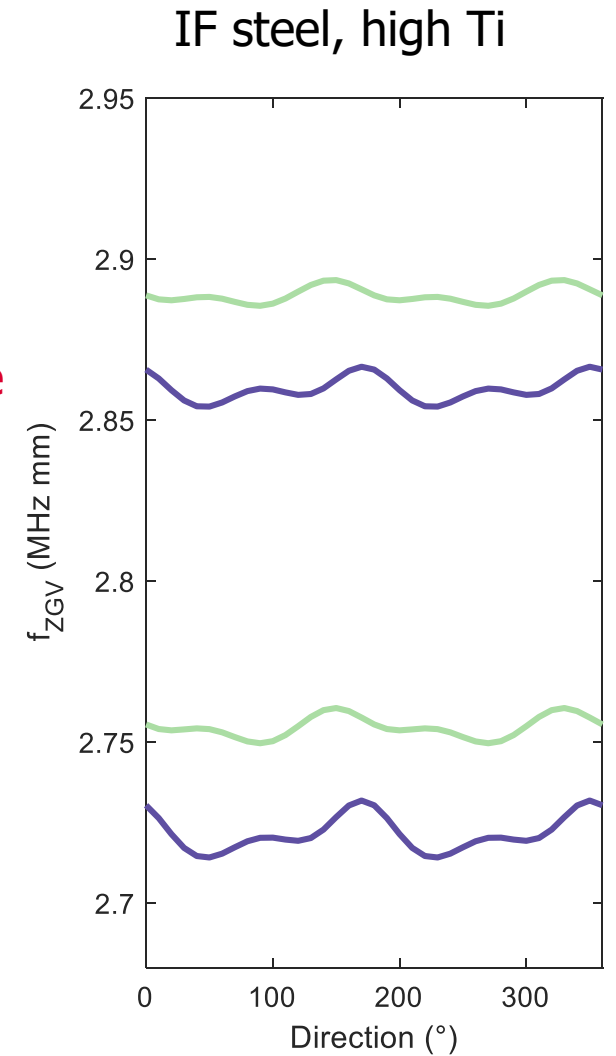
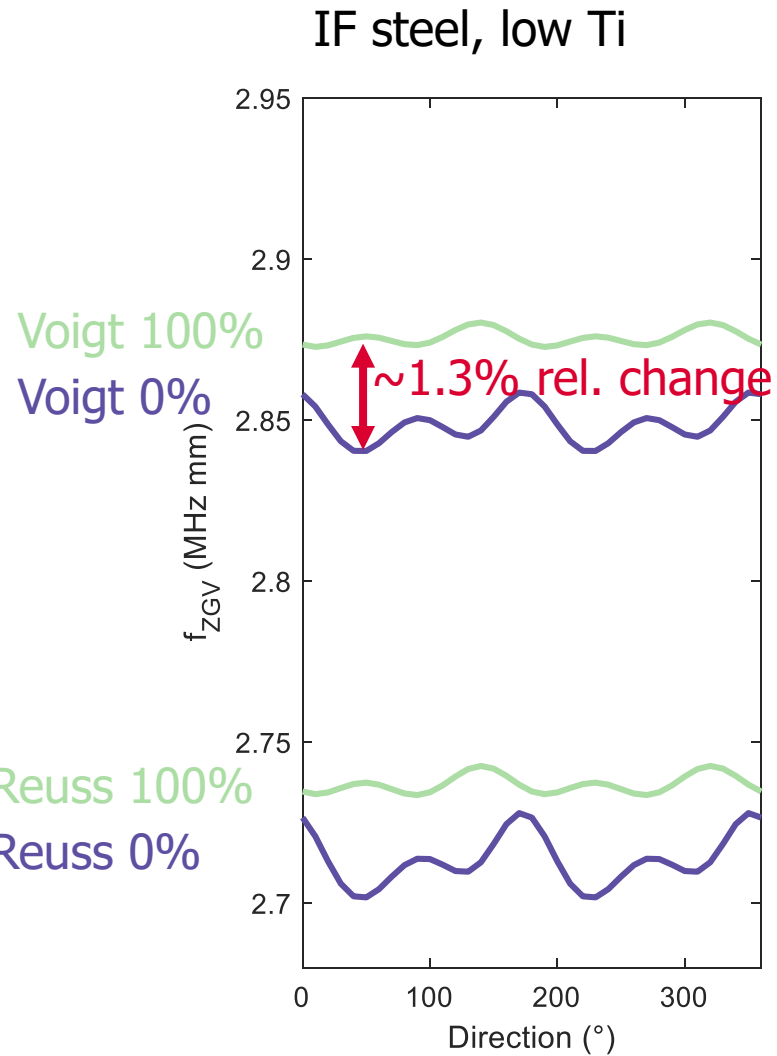
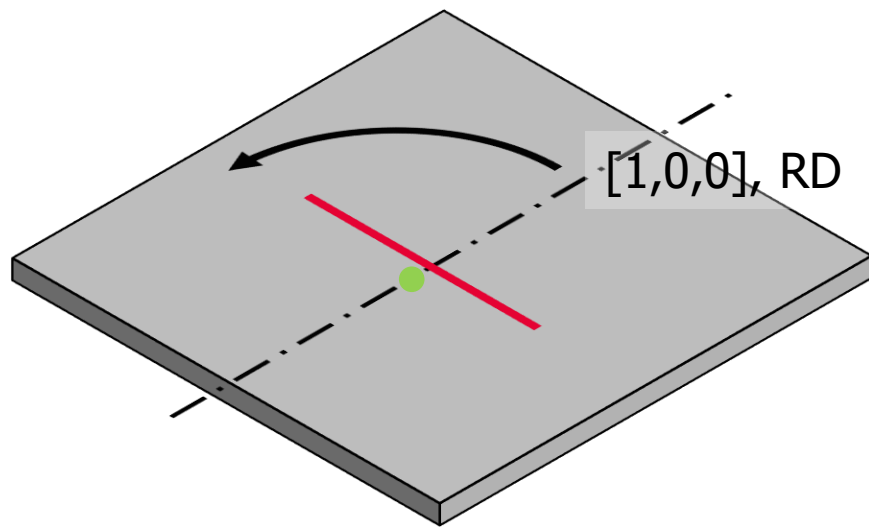
Other directions?

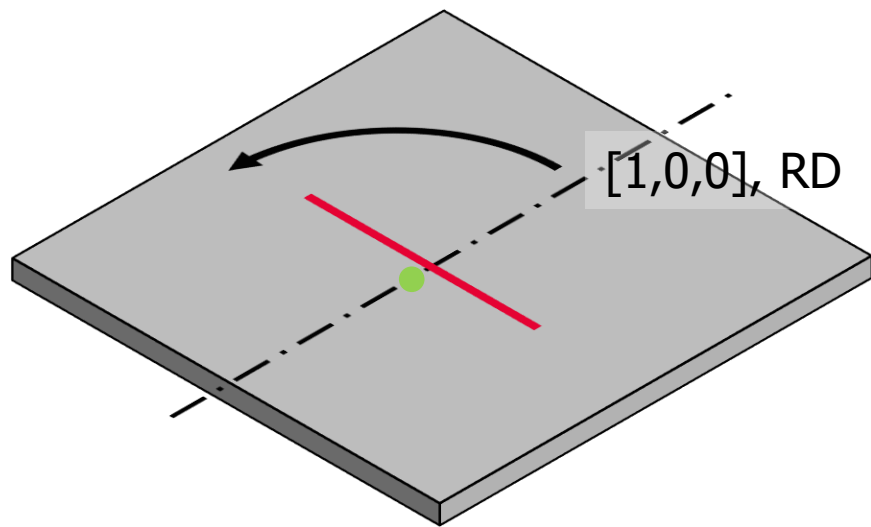
- changes of c_L in normal direction are small
- are other directions more sensitive?
- useful?



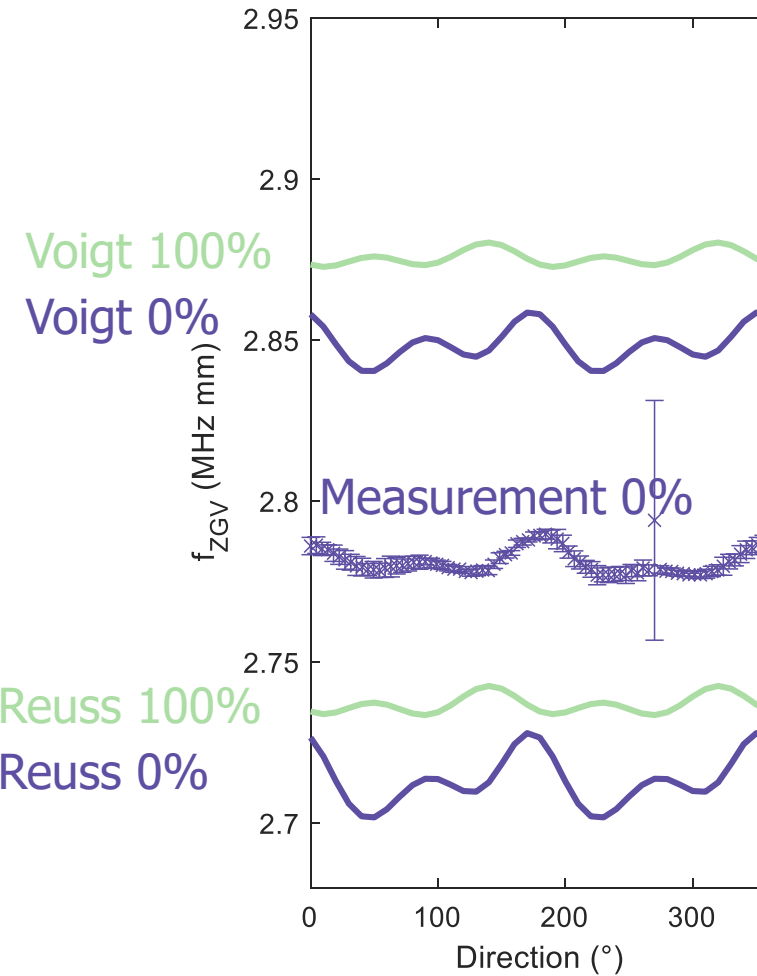
- ZGV resonances
- Surface Acoustic Waves
- Control propagation direction
- Same material properties?
- Additional information?
- SNR, ablation?



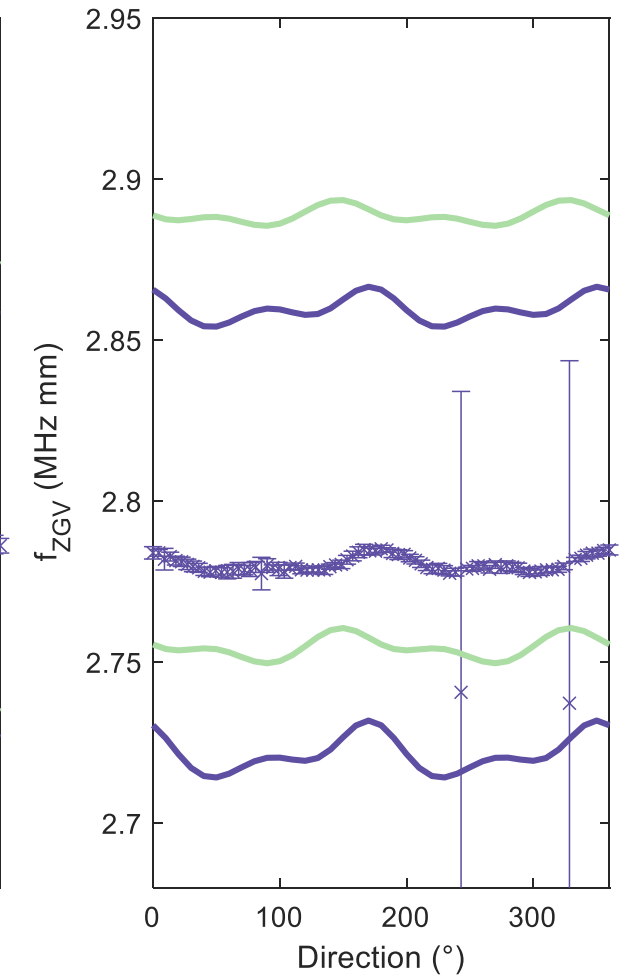


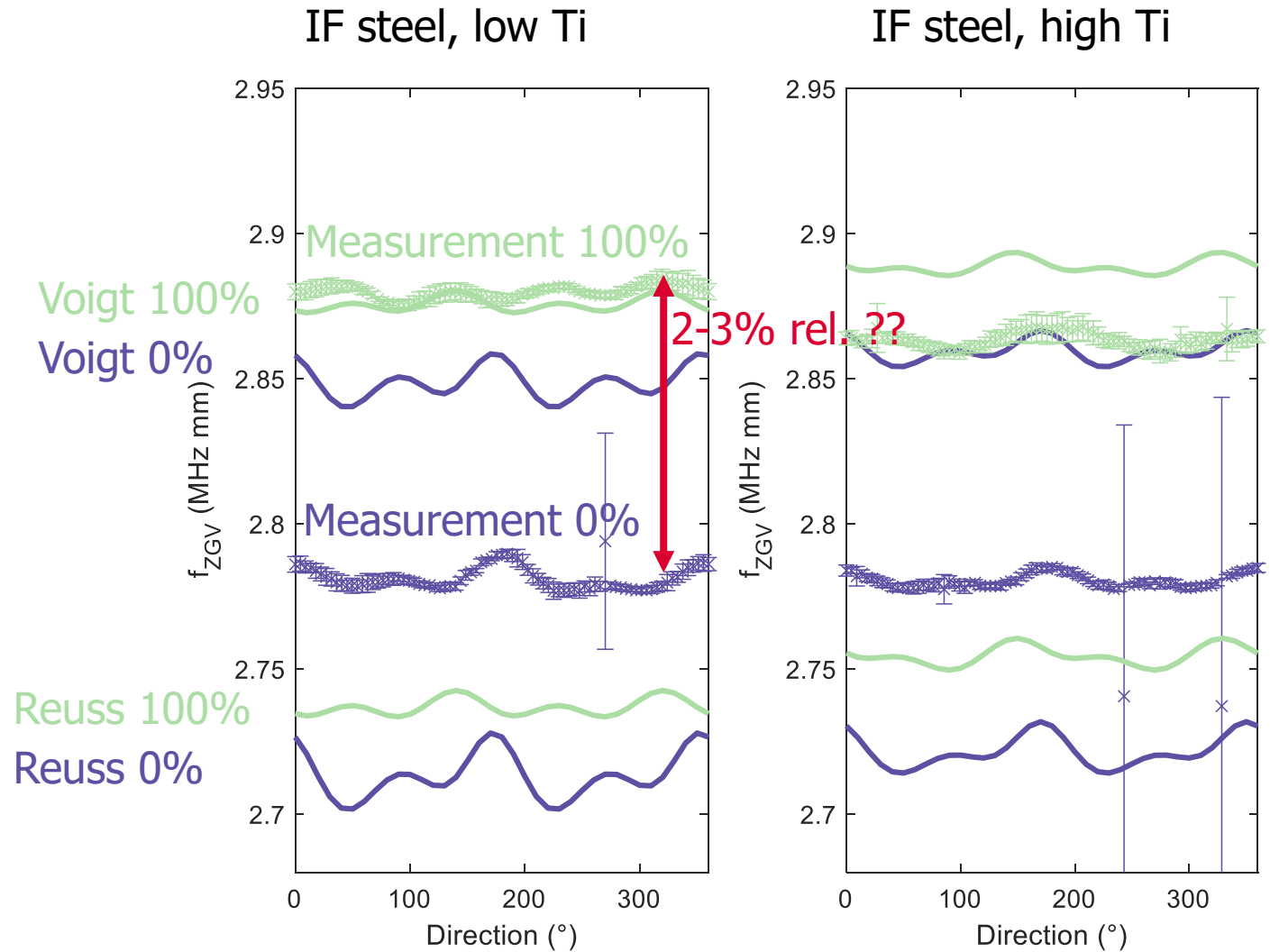
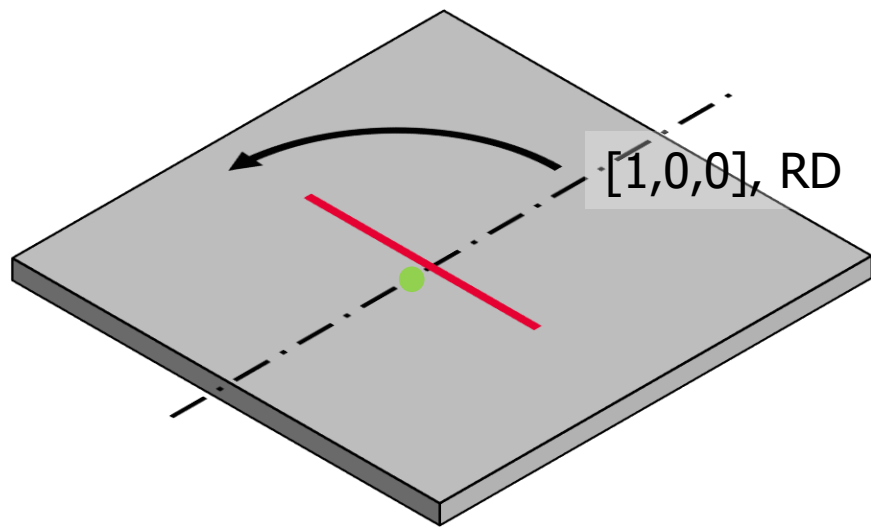


IF steel, low Ti



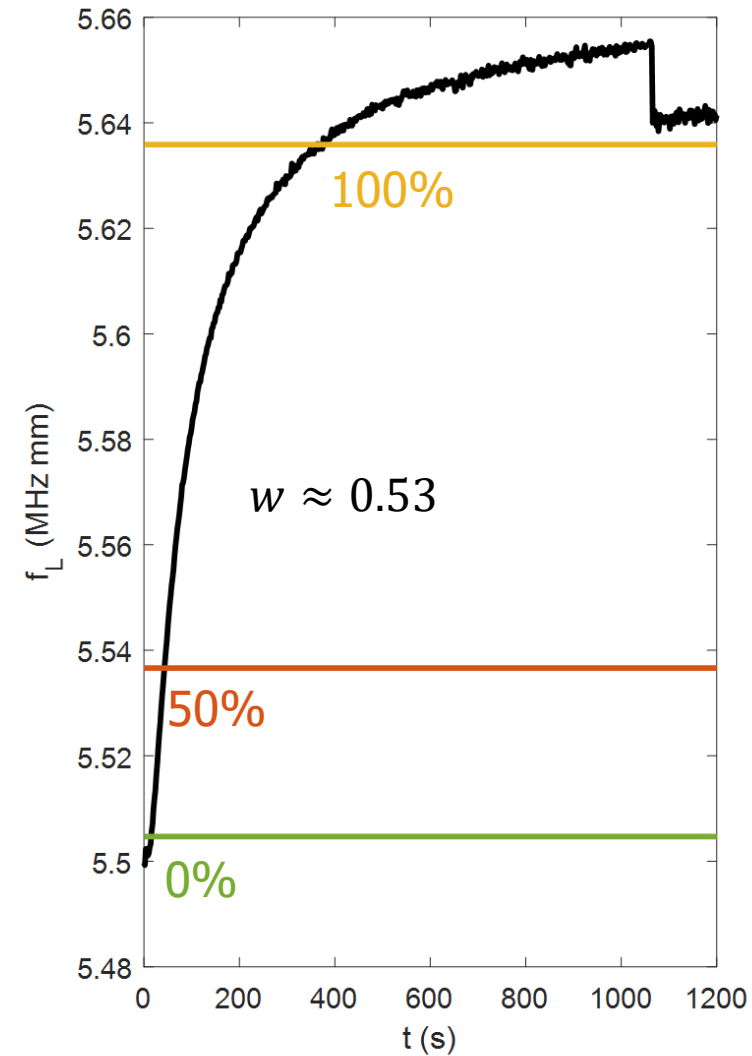
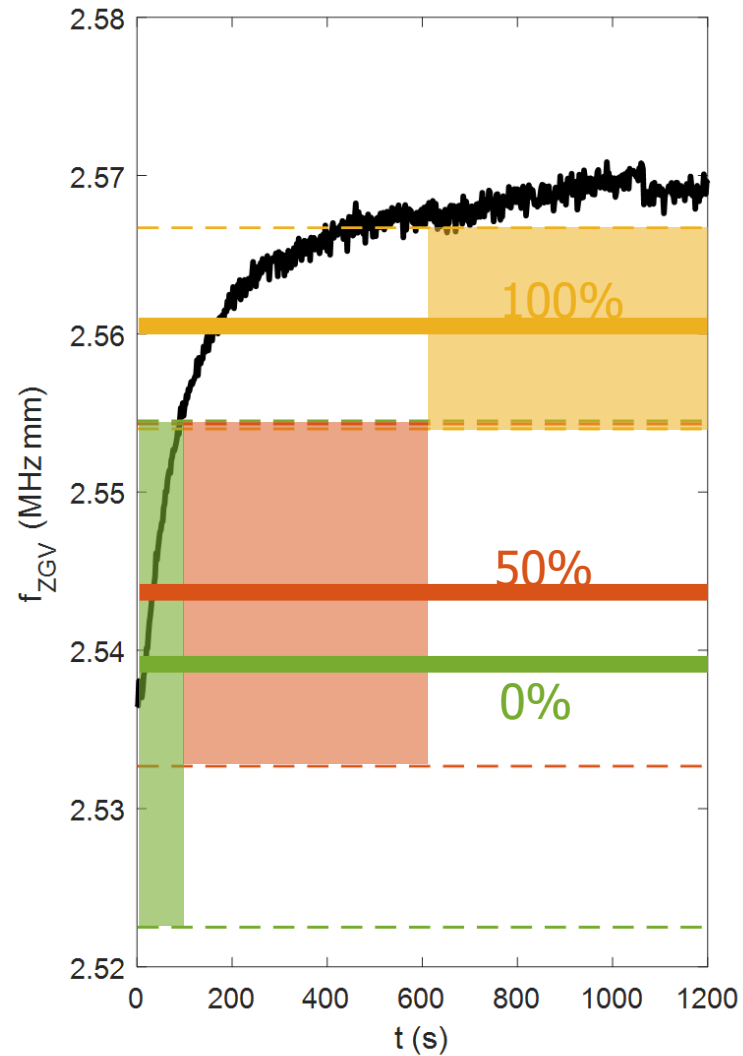
IF steel, high Ti



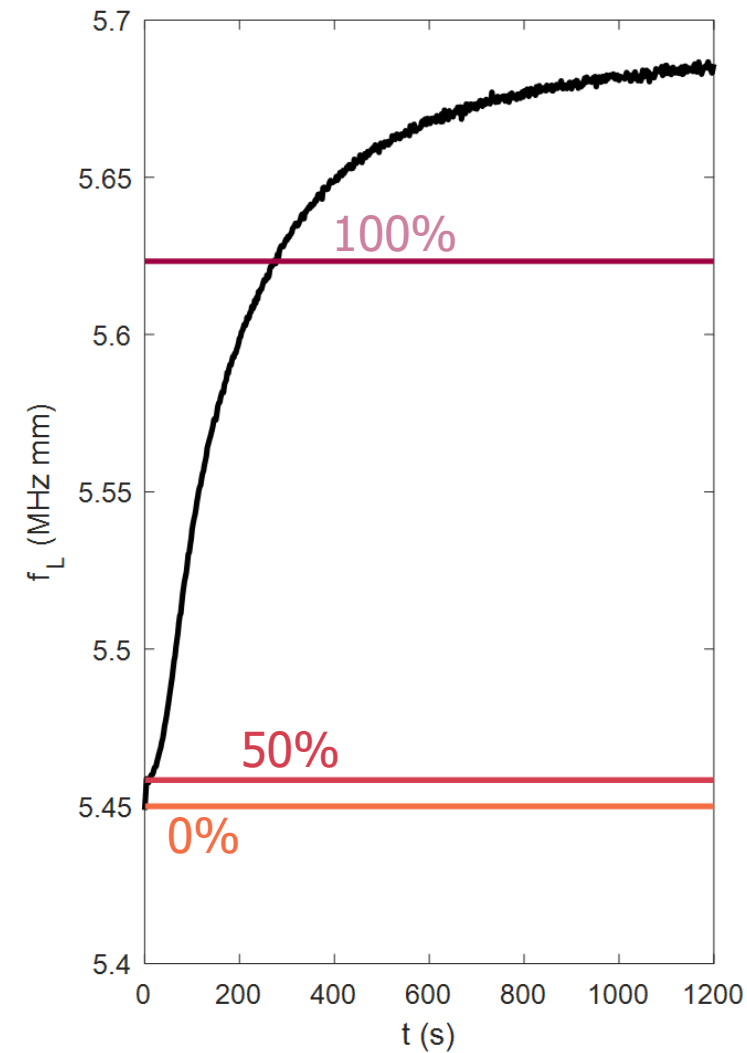
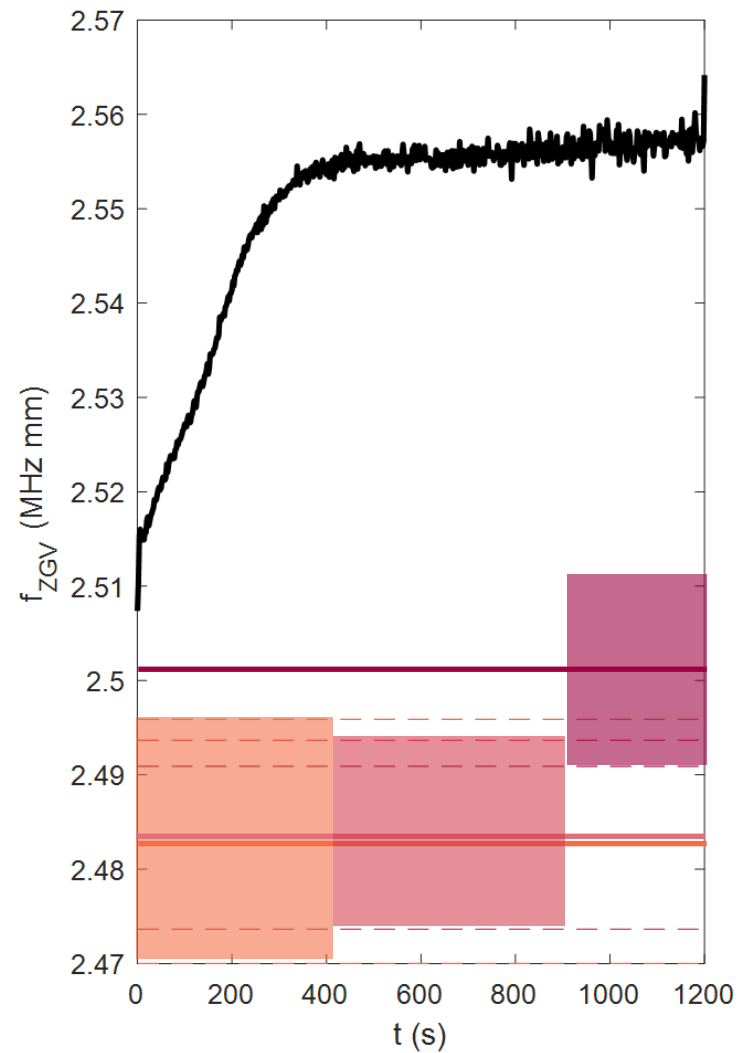


- Point source

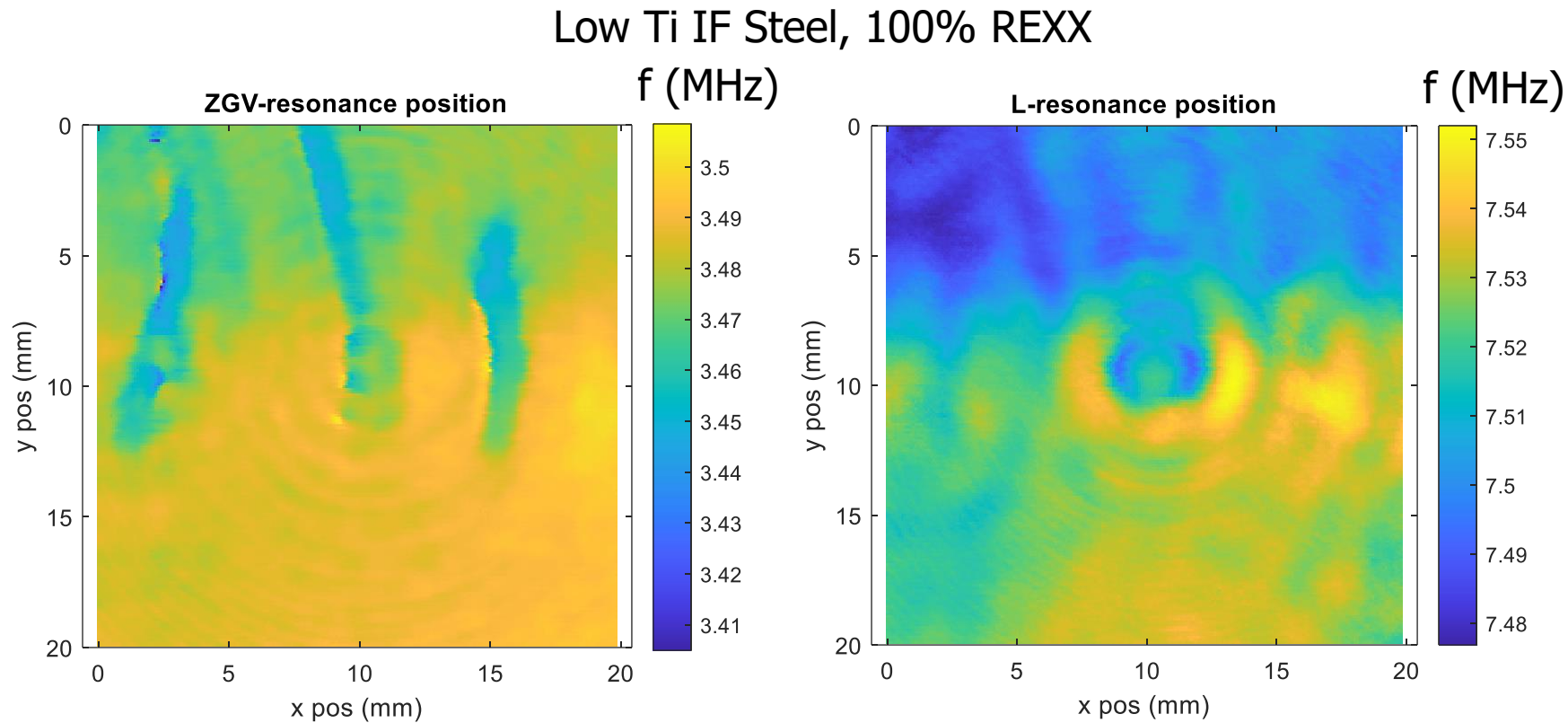
IF steel, low Ti, REXX at 600°C



IF steel, high Ti, REXX at 680°C

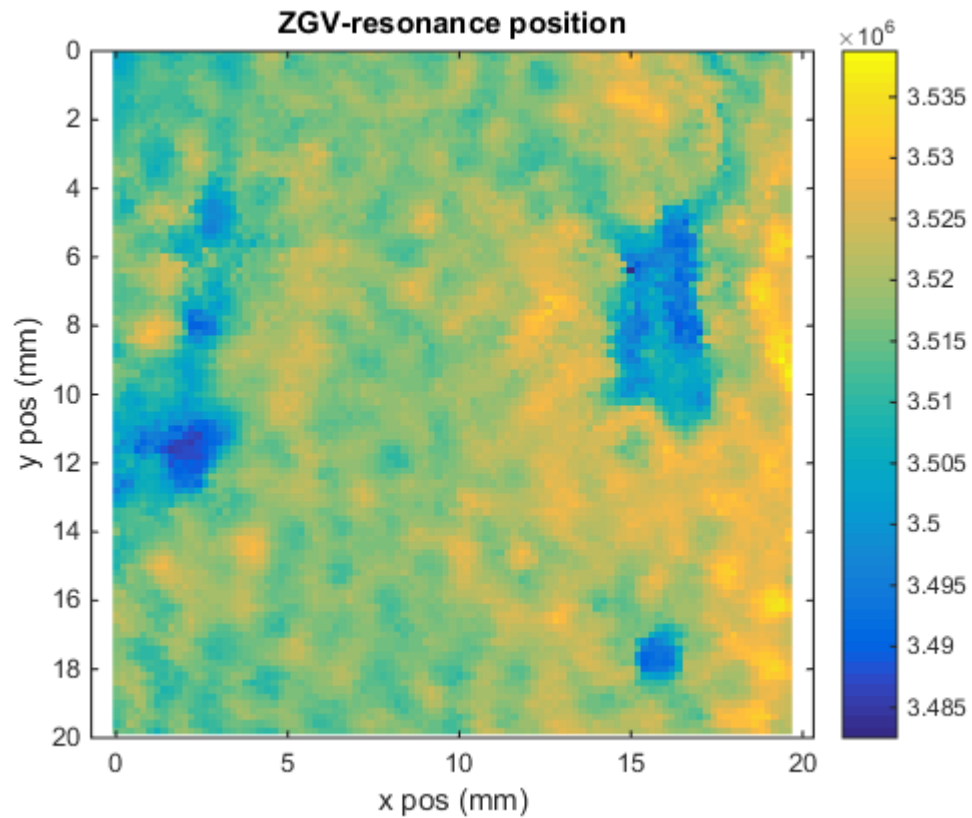


- ZGV resonances show local inhomogeneities



- Also visible in untreated (cold rolled) samples

Medium Ti IF Steel, 0% REXX



- Measured longitudinal sound velocity in situ on 0.8mm steel sheets, using plate resonances
- Calculated stiffness tensors from EBSD data (0%, 50%, 100% REXX)
- Good agreement of theory and experiment. Small shift of Reuss → Voigt observable?
- Extended to ZGV modes:
 - Ex situ: Good angular agreement, questions remain for 100% REXX
 - In situ: Depending on sample

Our work is funded by the
FFG Bridge program:

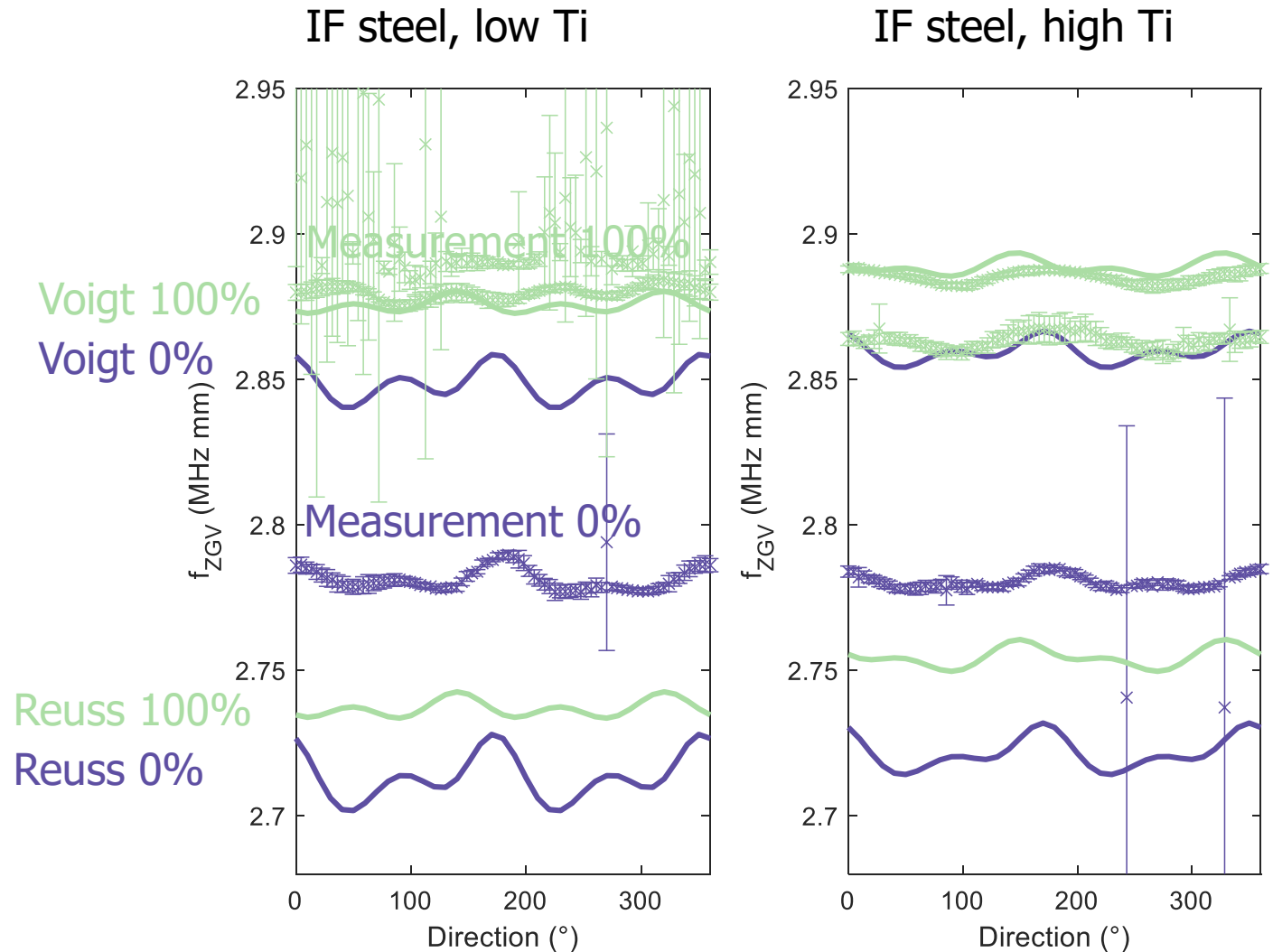
FO999901377 **STAHLUS**



Calculated vs. measured f_{ZGV} - ex situ

- Directional source (line)
- Rotate sample
- Line scan for each angle

■ ?



Calculated vs. measured f_{ZGV} - ex situ

- Directional source (line array)
- Rotate sample

